

⑫

EUROPEAN PATENT APPLICATION

⑲ Application number: 80301531.2

⑤① Int. Cl.³: **C 23 F 11/14**

⑳ Date of filing: 09.05.80

③⑨ Priority: 09.05.79 US 37418
10.04.80 US 138758

⑦① Applicant: Conner Sr., Alvin J., 19 Charlotte Drive, New Orleans, Louisiana 70122 (US)

④③ Date of publication of application: 10.12.80
Bulletin 80/25

⑦② Inventor: Conner Sr., Alvin J., 19 Charlotte Drive, New Orleans, Louisiana 70122 (US)

⑧④ Designated Contracting States: AT BE DE FR GB IT NL
SE

⑦④ Representative: Collier, Jeremy Austin Grey, J.A. Kemp & Co. 14, South Square Gray's Inn, London WC1R 5EU (GB)

⑤④ Non-petroleum based metal corrosion inhibitor and a metal object coated therewith.

⑤⑦ A non-petroleum based metal corrosion inhibitor is provided in the form of a solution of compounds mixed together in particular proportions to form a non-petroleum based coating for preventing, or inhibiting, the oxidation of metals. The solution is prepared from aliphatic mono-basic acids, aromatic acids, amines and water, with or without a lubricant. A coating of the solution inhibits oxidation of metal surfaces, provides lubricity and need not be removed from a metal surface prior to painting.

EP 0 020 042 A2

BEST AVAILABLE COPY

- 1 - TITLE MODIFIED
see front page

NON-PETROLEUM BASED
METAL CORROSION INHIBITOR

This invention relates to non-petroleum based metal corrosion inhibitors.

Description of the Prior Art

Metal industries and, particularly, the steel industry
5 are plagued with the problem of corrosion, e.g.,
rusting, of metal products, especially sheet products.
With the more refined methods of producing higher
grade steel sheets for use in automobiles, appliances
and allied industries, the problem of rusting during
10 the manufacturing process, storage and shipment has
become a significant one.

Various means have been and are being employed to
combat this problem. Inhibited petroleum based oils
are widely used as coatings for inhibiting the corrosion
15 of various steels. This type of protection, however,
is becoming increasingly impractical due to cost,
the hazardous conditions created by the use of the
petroleum based coatings, difficulty in removing the
coatings and difficulty in disposing of the oil
20 following its removal from the steel. Additionally,
so-called smudging is sometimes caused by the
polymerization and oxidation of petroleum based
inhibitor.

- 3 -

The composition according to the present invention is generally prepared as a concentrated aqueous solution containing from about 25 to about 65% by weight of the non-aqueous components. For application
5 to metal surfaces, this concentrate is generally diluted up to about 5 times with water, i.e., 5 parts of water to 1 part of the concentrate. The composition offers protection against oxidation to aluminum, zinc coated or galvanized steel, aluminum coated steel, tin plated steel,
10 stainless steel, high carbon electrical grade steel, cold rolled carbon steel and the like.

DESCRIPTION OF PREFERRED EMBODIMENTS

The non-petroleum based corrosion inhibiting composition according to the present invention, including
15 a preferred composition which contains a minor amount of a petroleum oil, appears to be an aqueous solution of a reaction mixture of the various components. The exact mechanism of the formation of the solution, however, is not known.

20 Relatively high molecular weight aliphatic, monobasic acids are employed in preparing the non-petroleum based composition according to the present invention. Aliphatic acids having from about 8 to about 20 carbon atoms have been found to be useful in preparing
25 the composition. These acids include fatty acids, both saturated and unsaturated, such as caprylic acid, palmitic acid, stearic acid, oleic acid and linoleic acid and resin acids such as abietic acid and acids isomeric therewith. These acids can be used alone or
30 in combination.

In a preferred embodiment of the invention, a mixture of tall oil fatty acids and rosin, because of its availability and cost and the properties of the resultant corrosion inhibiting composition, is used as
35 the high molecular weight aliphatic acid component of

- 4 -

the composition. Such mixtures are obtained as a byproduct of the paper industry from tall oil usually recovered from pine wood "black liquor". Oleic and linoleic acids are the major components of the tall oil fatty acids with acids such as palmitic acid, isostearic acid and stearic acid being present in relatively minor amounts. In a typical mixture of tall oil fatty acids and rosin useful in the present invention, oleic acid and linoleic acid comprise about 45% and 35% by weight, respectively, of the fatty acids. Rosin is mainly comprised of isomeric forms of abietic acid. The rosin can be present in amount of from about 5 to 40% by weight; preferably, 10 to 40% by weight, of the tall oil fatty acid/rosin mixture. Mixtures containing less than about 5% by weight of rosin cannot be used because of problems relating to viscosity. Increased amounts of rosin appear to decrease the viscosity of the corrosion inhibiting composition. Mixtures containing more than about 40% rosin are not economical.

Other mixtures of aliphatic acids such as tallow, the major constituents of which are oleic, palmitic, stearic, myristic and linoleic acids, can also be employed in preparing the non-petroleum based corrosion inhibiting compositions according to the present invention. The high molecular weight aliphatic, monobasic acid component of the corrosion inhibiting composition is employed in an amount of about 5 to 20 parts by weight based on about 100 parts by weight of the concentrated solution.

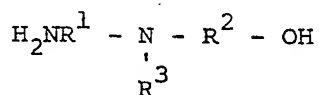
The composition according to the present invention typically contains a minor amount of a lubricant which may be either a petroleum or a non-petroleum product. Any of the petroleum oils presently employed in petroleum based corrosion inhibiting compositions for steel are believed to be useful in the

- 5 -

present composition. Good results have been obtained using a 100 SSU viscosity petroleum oil. In lieu of a petroleum oil, esters such as butyl stearate, dioctyl sebacate, butyl benzoate, or any of the light alkyl esters with boiling ranges above 350°F can be used as the lubricant. In a particularly preferred embodiment a petroleum oil is used as the lubricant. To obtain a stable aqueous solution of the composition the amount of lubricant is limited by the amount of the high molecular weight aliphatic acid. More particularly, the lubricant is employed in an amount of from about 10 to 20% of the aliphatic acid, i.e., 0.5 to 4 parts by weight per 100 parts by weight of the concentrated solution. Amounts of greater than about 20% are not completely solubilized in the composition.

In applications where lubrication requirements are not severe, the lubricant can be omitted from the metal corrosion inhibiting compositions. Such compositions will provide coatings which give good corrosion protection and which have a lubricity similar, for example, to soapy water. Such lubricity is believed to result from amine soaps or salts of the aliphatic and aromatic acids employed in the compositions.

The aminoalkylalkanolamine of the metal corrosion inhibiting compositions according to this invention has the following general structural formula:



wherein R^1 and R^2 are independently alkylidene of 1 - 4 carbon atoms and R^3 is hydrogen or alkyl of 1 - 4 carbon atoms. One or more of these aminoalkylalkanolamines can be employed in the non-petroleum based inhibitor composition according to the present invention.

- 6 -

Aminoethylethanolamine is presently preferred because of its cost and the good results that it provides. The specific use of the aminoalkylalkanolamine appears to be important to obtaining a stable lubricant-containing composition which is completely clear, will not stratify or separate and which can be diluted up to about 5 times its weight with water. The amount of the aminoalkyl-alkanolamine typically employed is 0.5 to 4 parts by weight per 100 parts by weight of the concentrated solution. Greater amounts are not required for stability and are not warranted from the standpoint of cost.

Where a lubricant is omitted from the metal corrosion inhibiting composition, the specific use of the aminoalkylalkanolamine does not appear to be required to obtain clear, stable solutions which provide good corrosion inhibiting coatings.

The metal corrosion inhibiting composition according to the present invention includes as a corrosion inhibitor a water-soluble amine salt of an aromatic acid. As the aromatic acid there may be employed an aromatic monocarboxylic acid such as benzoic acid or an aromatic polycarboxylic acid such as phthalic, isophthalic, terephthalic or trimellitic acid. Mixtures of the aromatic acids may also be employed. Although it has not been confirmed, it is believed that the aromatic acids may also contain other functional groups such as hydroxy and lower alkyl groups which do not inhibit the formation of the water-soluble salt. Good corrosion inhibiting effects have been obtained employing about 10 to 35 parts and, particularly, 24 to 35 parts of the aromatic acid per 100 parts by weight of the concentrated solution.

Virtually any primary, secondary, tertiary or cyclic amine which forms the water-soluble salt with the aromatic acid can be used in the composition

- 7 -

according to the present invention to provide corrosion inhibiting properties. Particularly good results have been obtained with the use of (lower C_2-C_4) alkanol- amines and, particularly, monoethanolamine and diethanolamine. Other suitable amines are triethanol, diisopropylamine, cyclohexylamine and morpholine. The amines can be used alone or in combination. The amines employed in the metal-corrosion inhibiting composition according to the present invention also serve to neutralize the aliphatic acid and appear to assist in the solubilization of the lubricant component. The total amount of amines employed in the composition, including the amount of aminoalkylalkanolamine, therefore, is generally in slight excess of the amount required to neutralize, i.e., form salts with, the aliphatic and aromatic acids. Depending on the amounts of the aliphatic and aromatic acids employed, this amount of the amine component is typically within the range of 5 to 25 parts by weight per 100 parts by weight of the concentrated solution. In preferred embodiments the amount is within the range of 15 to 20 parts by weight per 100 parts by weight of the concentrate.

Although the total amount of the high molecular weight aliphatic monobasic acid, lubricant, aromatic acid and salt-forming amines can vary within the ranges described above, for practical use as a concentrate, the non-aqueous components of the compositions are employed in an amount of from 25 to 65 parts per 100 parts by weight of the concentrate. In particularly preferred compositions, the non-aqueous components are employed in an amount of from 55 to 65 parts per 100 parts by weight of the concentrate; the remainder of the concentrate being water. To facilitate application of the corrosion inhibiting compositions to the metal surfaces, the concentrated solutions are

- 8 -

diluted up to 5 times, preferably about 4 times, with water, i.e., up to 500 parts of water per 100 parts of the concentrate.

5 The sequence of addition of the various components appears to be important to get a finished product which is clear, stable and which can be diluted to produce a stable product for final use.

10 Generally, the mixture of the above-described aliphatic, monobasic acid component and lubricant are added to water with stirring in a suitable mixing device. This is followed by the addition of the aminoalkylalkanolamine which causes the formation of a cloudy emulsion. An amount of the amine (which

- 9 -

forms the water-soluble salt with the aromatic acid) in excess of that required to form a clear solution from the cloudy emulsion is then added followed by the aromatic acid and the remainder of the salt-forming amine. In another variation, a solution of the aromatic acid and salt-forming amine can be added to a solution of the aliphatic acid - lubricant - aminoalkylalkanolamine. A unique characteristic of the present invention is that following these procedures, a lubricant, either natural or synthetic, can be completely solubilized in water when the amounts of the components of the non-petroleum based inhibitor concentration are maintained within the ranges described above.

The preparation of typical 55 gallon (208 litre) batches of concentrated solution of the non-petroleum based corrosion inhibitor is described below (approximate weights are in parenthesis):

- (1) Pump 30 gallons of water (250 lbs)(114 litres, 113 kg.) at 120°F (49°C) into tank and agitate. Add 10 gallons (38 litres) of a tall oil fatty acid/rosin mixture (80 lbs)(36 kg) sold under the tradename Unitol-DT-40 by Union Camp and 1 or 2 gallons (3.8 or 7.6 litres) of 100 SSU viscosity petroleum oil (7-14 lbs)(3.2 - 6.4 kg) The oil will dissolve in the tall/oil-rosin

- 10 -

5 mixture, but neither the petroleum oil
not the tall oil fatty acid/rosin mixture
will dissolve in water. While agitating add
one gallon of aminoethylethanolamine (8 lbs)
(3.6 kg). An oil in water emulsion will
form. This emulsion is milky and complete-
ly opaque. Add 8 gallons (30 litres)
of monoethanolamine (64 lbs)(29 kg.) and
the mixture will become clear and stable.
10 Add 100 pounds (45 kg.) of benzoic acid and
the mixture will become hazy because of the
portion of the benzoic acid which has not
been neutralized to a soluble salt. To
complete neutralization of the benzoic acid,
15 add more monoethanolamine (or morpholine,
cyclohexylamine, etc.) until the solution is
completely clear and has a pH of 8.0 to 9.5.
Continue mixing for 30 minutes and recheck
pH. If pH drops below 8.0, add more mono-
ethanolamine to bring pH to 9.0.
20 (2) Dump 30 gallons of water (250 lbs)(114
litres, 113 kg) at 110 - 120°F (43 - 49°C)
into a tank, add 10 gallons (38 litres) of
tall oil fatty acids containing 8 - 12%
rosin acids. While agitating, add one
25 quart of aminoethylethanolamine. The tall

- 11 -

oil/rosin mixture will emulsify (solution will be milky). Then add 2 1/2 gallons (9.5 litres) of diethanolamine and the solution will clear and thicken. While agitating slowly add 45 pounds (20 kg.) of terephthalic acid. The solution will remain clear and the viscosity will drop. Dilute up to 55 - 58 gallons (208 - 220 litres) with water and continue agitating until all the terephthalic acid has dissolved. The viscosity of the finished solution at 100°F (38°C) will be about the same as a 30 wt commercial grade lubricating oil.

For use at the mills or manufacturing plants, a composition prepared as described above is diluted with up to 5 parts of water and applied as either a rust preventative and/or lubricant. The recommended dilution ratio is 1 part concentrate to about 4 parts water.

Preferred compositions according to the present invention are formed by the sequential addition of the following compounds to 250 lbs (about 30 gallons; 113 kg, 114 litres) of water with stirring (weights are approximate):

- 12 -

	(a)	tall oil fatty acids/rosin	80 lbs (36 kg)
	(b)	petroleum oil (100 SSU viscosity)	7 - 14 lbs (3.2 - 6.4 kg)
	(c)	aminoethylethanolamine	8 lbs(3.6kg)
	(d)	monoethanolamine	16 lbs(7.3kg)
5	(e)	benzoic acid	150 - 200 lbs (68 - 91 kg)
	(f)	monoethanolamine	75 - 100 lbs! (34 - 45 kg)
	and		
	(a)	tall oil fatty acids/rosin	40 lbs (18kg)
10	(b)	petroleum oil	3.5 - 7 lbs (1.6 -,3.2 kg)
	(c)	aminoethylethanolamine	41 lbs (19kg)
	(d)	monoethanolamine	8 lbs(3.6kg)
	(e)	benzoic acid	150 - 200 lbs (68 - 91kg)
	(f)	monoethanolamone	50 - 75 lbs (23 - 34 kg)
15	(g)	diethanolamine	43 lbs(19.5kg)

The above formulations use only 1 or 2 gallons (3.8 or 7.6 litres) of petroleum oil per fifty-five gallon (208 litre) batch of concentrate. When the concentrated solution is diluted four to one with water, it acts as a direct replacement for oil and replaces up to 200 gallons (757 litres) solution. Actual tests have shown that when used as a replacement for oil, one quart (1 litre) of the solution replaces two gallons (7.6 litres) of oil, so the overall use of oil by steel mills is reduced consider-

- 13 -

ably.

With the cost of petroleum increasing dramatically
the savings through the use of the compositions
described herein are _____

- 14 -

considerable. Also, large quantities of petroleum can be released for more important uses.

Another advantage of this solution over petroleum-based inhibitors is that the petroleum-based compositions must be removed from the steel before it can be painted. When degreasing is performed, chlorinated solvents, such as trichloroethylene or perchloroethylene are used. Both are suspected carcinogens and usage of each is now restricted. EPA and OSHA have severely reduced the permissible limits of these substances in the atmosphere. Degreasing is also expensive. Oil disposal also presents an expensive problem. When washing is exercised to remove the oil, detergents and caustic solutions must be used. The wash water and oil cannot be discharged into the drainage systems.

The composition according to the present invention does not have to be removed from the surface of metals prior to painting in most cases. However, when it must be removed, water will remove it from the surface. The water can be discharged into drains since the solution is biodegradable.

The application of the petroleum-based inhibitor compositions at the mills creates further hazards because for every gallon of oil which is applied, some will drip off and create unsafe working conditions. When the oil is applied to sheets which are coiled, oil is spread throughout the area because of the centrifugal motion of the coiling operation. Solvents are used to clean the work area, which may create additional hazards. These operations are eliminated with the use of the non-petroleum based corrosion inhibiting compositions according to the present invention.

When employed in a steel making operation, the inhibitor composition of the present invention should be applied after pickling and hot roll reduction

- 15 -

operations, and prior to cold reduction, because the cleaned pickled sheet is very susceptible to rusting. Reapplication of the composition after the final reduction protects the coils during storage prior to annealing. The composition can be reapplied at the temper mill operation, either on the entry or exit side of the temper mill. When the composition is applied at the entry side, a very fine mist application is desirable so as not to cause problems on the temper mill rolls. The composition is applied at the exit side of the temper mill either as a light or heavy spray. This also applies when the solution is applied at the stretch or shear line.

Tests in a humidity cabinet or on coils stored for two months show that the protection afforded by the non-petroleum based corrosion inhibitor composition of the present invention is as good, or better, than conventional inhibited oils.

EXAMPLES

To illustrate the corrosion inhibiting properties of the non-petroleum based corrosion inhibitor compositions according to the present invention when applied to steel, the following compositions were prepared according to the general procedures described above. In the compositions, percentages are by weight and the tall oil fatty acids/rosin mixtures employed are commercially available compositions in which the fatty acids are _____

- 16 -

composed primarily of a mixture of oleic and linoleic acids:

5	(1)	(a)	Tall oil fatty acid (TOFA) 60%; rosin 40%	12 - 18%
		(b)	100 SSU Vis Petroleum Oil	2 - 4%
		(c)	Amine mixture: 40% aminoethylethanolamine (AEE), 60% monoethanolamine (MEA)	5 - 10%
		(d)	Benzoic acid	10 - 20%
		(e)	Water	71 - 48%
10	(2)	(a)	TOFA 60%; rosin 40%	12 - 18%
		(b)	100 SSU Sec Petroleum Oil	2 - 4%
		(c)	Amine mixture: 40% AEE, 50% MEA, 10% morpholine	5 - 10%
		(d)	Benzoic acid	10 - 20%
		(e)	Water	71 - 48%
15	(3)	(a)	TOFA 70%; rosin 30%	12 - 18%
		(b)	100 SSU Sec Petroleum Oil	2 - 4%
		(c)	Amine mixture: 30% AEE, 70% MEA	5 - 10%
		(d)	Benzoic acid	10 - 20%
		(e)	Water	71 - 48%
20	(4)	(a)	TOFA 80%; rosin 20%	12 - 18%
		(b)	100 SSU Sec Vis Petroleum Oil	2 - 4%
		(c)	Amine mixture: 30% AEE, 70% MEA	5 - 10%
		(d)	Benzoic acid	10 - 20%
		(e)	Water	71 - 48%
25				

- 17 -

5	(5)	(a)	Oleic acid 80%; rosin - abietic acid 20%	12 - 18%
		(b)	100 SSU Vis Petroleum Oil	2 - 4%
		(c)	Amine mixture: 30% AEE, cyclohexylamine 70%	5 - 10%
		(d)	Benzoic acid	10 - 20%
		(e)	Water	71 - 48%
10	(6)	(a)	Caprylic acid 70%; abietic acid 30%	12 - 18%
		(b)	100 SSU Sec Vis Petroleum Oil	2 - 4%
		(c)	30% AEE, 70% MEA	5 - 10%
		(d)	Benzoic acid	10 - 20%
		(e)	Water	71 - 48%
15	(7)	(a)	TOFA 80%; rosin 20%	12 - 18%
		(b)	Butyl Stearate	2 - 4%
		(c)	30% AEE, 70% MEA	5 - 10%
		(d)	Benzoic acid	10 - 20%
		(e)	Water	71 - 48%
20	(8)	(a)	Tallow Fatty Acid	12 - 18%
		(b)	100 SSU Sec Vis Petroleum Oil	2 - 4%
		(c)	30% AEE, 70% MEA	5 - 10%
		(d)	Benzoic acid	10 - 20%
		(e)	Water	71 - 48%
25	(9)	(a)	Tallow Fatty Acid 80%; rosin 20%	12 - 18%
		(b)	100 SSU Sec Vis Petroleum Oil	2 - 4%
		(c)	30% AEE, 70% MEA	5 - 10%
		(d)	Benzoic acid	10 - 20%
		(e)	Water	71 - 48%

- 18 -

5	(10)	(a)	TOFA 70%; rosin 30%	12 - 18%
		(b)	100 SSU Sec Vis Petroleum Oil	2 - 4%
		(c)	20% AEE, 80% diethanolamine	5 - 10%
		(d)	Benzoic acid	10 - 20%
		(e)	Water	71 - 48%
10	(11)	(a)	TOFA 70%; rosin 30%	12 - 18%
		(b)	100 SSU Sec Vis Petroleum Oil	2 - 4%
		(c)	10% AEE; 90% diethanolamine	5 - 10%
		(d)	Benzoic acid	10 - 20%
		(e)	Water	71 - 48%
15	(12)	(a)	TOFA 70%; rosin 30%	12 - 18%
		(b)	100 SSU Sec Vis Petroleum Oil	2 - 4%
		(c)	Diethanolamine	5 - 10%
		(d)	Benzoic acid	10 - 20%
		(e)	Water	71 - 48%
20	(13)	(a)	TOFA 90%; rosin 10%	12 - 18%
		(b)	Amine mixture: 10% AEE; 90% diethanolamine (DEA)	5 - 10%
		(c)	Terephthalic acid (TPA)	10 - 20%
		(d)	Water	73 - 52%
	(14)	(a)	TOFA 90%; rosin 10%	12 - 18%
25		(b)	DEA	5 - 10%
		(c)	TPA	10 - 20%
		(d)	Water	73 - 52%
	(15)	(a)	TOFA 90%; rosin 10%	12 - 18%
		(b)	Amine mixture: 10% AEE; 90% MEA	5 - 10%

- 19 -

	(c)	Phthalic acid (PA)	10 - 20%
	(d)	Water	73 - 52%
5	(16)	(a) TOFA 90%; rosin 10%	12 - 18%
		(b) MEA	5 - 10%
		(c) Isophthalic acid (IPA)	10 - 20%
		(d) Water	73 - 52%
	(17)	(a) Oleic acid	12 - 18%
		(b) Triethanolamine (TEA)	5 - 10%
		(c) IPA	10 - 20%
10		(d) Water	73 - 52%
	(18)	(a) Neodecanoic acid	12 - 18%
		(b) Amine mixture:	
		10% AEE; 90% DEA	5 - 10%
		(c) TPA	10 - 20%
15		(d) Water	73 - 52%
	(19)	(a) Tallow fatty acid	12 - 18%
		(b) 100 SSU Sec Vis Petroleum Oil	2 - 4%
		(c) Amine mixture:	
		30% AEE; 70% MEA	5 - 10%
20		(d) IPA	10 - 20%
		(e) Water	71 - 48%
	(20)	(a) TOFA 80%; rosin 20%	12 - 18%
		(b) Amine mixture:	
		30% morpholine; 70% diethanol- amine	5 - 10%
25		(c) TPA	10 - 20%
		(d) Water	73 - 52%

- 20 -

- (21) (a) TOFA 95%; rosin 5% 5 - 10%
(b) Neodecanoic acid 9 - 12%
(c) Amine mixture:
30% morpholine; 70% DEA
5 (d) TPA 10 - 20%
(e) Water 71 - 48%

These compositions were evaluated for corrosion inhibiting properties according to the testing procedures described below. Data for other corrosion
10 inhibiting compositions are presented for comparative purposes.

TESTING PROCEDURE

Cold roll dry strips (1 1/4", 3.2cm. wide by 4", 10.2cm. long, dry, clean and rust-free) were
15 used as test specimens. A 1/16" (1.5mm.) hole was punched 1/8" (3.2 mm.) from the top and bottom, and 5/8" (1.6 cm.) from one side. A hook, fabricated from galvanized wire, was used to hang the strips in a humidity cabinet. Each strip was marked for
20 identification by embossing a number with a metal stamp about 1/4" (6.4mm.) below the punched hole. To standardize the test, a strip as described above was dipped 2" (5cm.) in the solution to be tested and suspended by a metal hook with the dipped or
25 coated portion of the strip at the bottom.

- 21 -

The strip was allowed to dry or drain for one hour, and the hook transferred to the opposite end of the strip, which was then suspended on a rack in the humidity cabinet. The coated or dipped end was now on top, and the lower, uncoated end of the strip on the bottom. The conditions in the humidity cabinet were maintained a 100°F (38°C) and 100% humidity.

- 22 -

Observations of the strip were made every 24 hours. The lower or dry parts of all strips were completely rusted after 24 hours. All tests were run for 120 hours.

The condition of the coated parts were graded as follows:

5

- A. Completely free of rust
- B. Slight rusting on the surface, but less than approximately 2%
- C. Rust on approximately 5 - 10% of the area
- D. Completely rusted

SOLUTIONS TESTED		HOURS IN HUMIDITY CABINET				
		24	48	72	96	120
10	Lubricating - Preservative Oil MIL-L-2160A - Gr 2	A	A	A	A	A
	Lubricating - Preservative Oil MIL-L3150 - Gr 2	A	A	A	A	A
	Solvent Cutback MIL-O-16173 - Gr 2	A	A	A	A	A
	Uninhibited - 10 Weight Lubricating Oil	A	A	A	B	C
15	10% Solution - Sodium Nitrite 90% Distilled Water	A	B	B	C	D
	10% Solution - Sodium Benzoate 90% Distilled Water	A	B	C	C	D
	10% Ammonium Benzoate 90% Distilled Water	A	B	C	D	D
	10% Sodium Molybdate 90% Distilled Water	A	B	C	C	D
	10% Dicyclohexylamine Benzoate 90% Isopropyl alcohol	A	A	B	B	C
	10% Monoethanolamine Benzoate 90% Distilled Water	A	A	A	B	B
	10% Diethanolamine Benzoate 90% Distilled Water	A	A	B	B	B
	10% Diethanolamine Benzoate 90% Distilled Water	A	A	B	B	B
20	10% Diethanolamine Benzoate 90% Distilled Water	A	A	B	B	B

- 23 -

SOLUTIONS TESTED		HOURS IN HUMIDITY CABINET				
		24	48	72	96	120
5	Composition No. 1 100%	A	A	A	A	A
	Composition No. 1 25%					
	Deionized Water 75%	A	A	A	A	A
	Composition No. 2 25%					
	Deionized Water 75%	A	A	A	A	A
	Composition No. 3 25%					
	Deionized Water 75%	A	A	A	A	A
	Composition No. 4 25%					
	Deionized Water 75%	A	A	A	A	A
	Composition No. 5 25%					
	Deionized Water 75%	A	A	A	A	A
	Composition No. 6 25%					
	Deionized Water 75%	A	A	A	A	A
10	Composition No. 7 25%					
	Deionized Water 75%	A	A	A	A	A
	Composition No. 8 25%					
	Deionized Water 75%	A	A	A	A	A
	Composition No. 9 25%					
	Deionized Water 75%	A	A	A	A	A
15	Composition No. 10 25%					
	Deionized Water 75%	A	A	A	A	A
	Composition No. 11 25%					
	Deionized Water 75%	A	A	A	A	A
	Composition No. 12 25%					
	Deionized Water 75%	A	A	A	A	A
	Composition No. 13 100%	A	A	A	A	B
	Composition No. 14 100%	A	A	A	B	B
	Composition No. 15 100%	A	A	A	B	B
	Composition No. 16 60%					
	Deionized Water 40%	A	A	A	A	B

- 24 -

SOLUTIONS TESTED		HOURS IN HUMIDITY CABINET				
		24	48	72	96	120
Composition No. 17	80%					
Water	20%	A	A	A	A	A
Composition No. 18	100%	A	A	A	A	A
Composition No. 19	60%					
Water	40%	A	A	A	A	B
Composition No. 20	100%	A	A	A	A	B
Composition No. 21	100%	A	A	A	A	A

5

- 25 -

CLAIMS

1. A non-petroleum based metal corrosion
inhibiting composition consisting essentially of a
solution of one part by weight of a aqueous concentr-
ate and 0 to five parts by weight of water, said
5 aqueous concentrate being a solution comprising,
per 100 parts by weight of the concentrate, the
product of mixing

- 10 (a) 5 to 20 parts by weight of an
aliphatic, monobasic acid having
from 8 to 20 carbon atoms;
- (b) 0 to 4 parts by weight of a
lubricant;
- 15 (c) 10 to 35 parts by weight of an
aromatic mono or polycarboxylic
acid; and
- (d) an amine which forms a water
soluble salt with the aliphatic
and aromatic acids.

2. A non-petroleum based metal corrosion
20 inhibiting composition according to claim 1 where-
in the said aqueous concentrate is a solution comp-
rising, per 100 parts by weight of the concentrate,
the product of mixing in an aqueous medium;

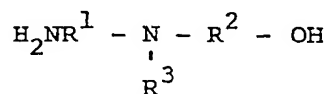
- 25 (a) 5 to 20 parts by weight of an

- 26 -

aliphatic, monobasic acid having
from 8 to 20 carbon atoms;

(b) 0.5 to 4 parts by weight of a
lubricant;

5 (c) an alkylaminoalkanolamine of the
formula:



10 where R^1 and R^2 are independently
alkylene of 1 - 4 carbon atoms,
and R^3 is hydrogen or alkyl of
1 - 4 carbon atoms;

(d) 10 to 35 parts by weight of an
aromatic mono~~or~~ polycarboxylic
acid; and

15 (e) an amine which forms a water-
soluble salt with the said aromatic
acid,

The amount of amines (c) and (e) being in slight
excess of that necessary to neutralize the aliphatic
20 and aromatic acids (a) and (d).

3. The composition of Claim 2 wherein the
amount of the alkylaminoalkanolamine (c) of the
concentrate is 0.5 to 4 parts by weight.

4. The composition of Claim 2 or 3 wherein,
25 the said alkylaminoalkanolamine (c) aminoethyle-

thanolamine.

5. The composition of any of Claim 2 to 4 wherein the amine (e) is an alkanolamine in which the alkyl group has 2 - 4 carbon atoms, cyclohexylamine, diisopropylamine, or morpholine.

6. The composition of any of Claims 2 to 5 wherein the lubricant (b) is a petroleum oil or an ester.

7. The composition of Claim 6 wherein the lubricant (b) is a 100 SSU viscosity petroleum oil.

8. The composition of any one of Claims 2 to 7 wherein the amounts of the components of said aqueous concentrate, per 100 parts by weight of the concentrate, are:

- (a) 5 to 20 parts by weight,
- (b) 0.5 to 4 parts by weight,
- (c) 0.5 to 4 parts by weight,
- (d) 24 to 35 parts by weight and
- (e) 15 to 20 parts by weight.

9. The composition of any one of Claim 2 to 8 wherein the total amount of components (a), (b), (c) (d) and (e) of said aqueous concentrate is 25 to 65 parts per 100 parts by weight of concentrate, the remainder being water.

10. The composition of Claim 9 wherein the total

amount of components (a), (b), (c), (d) and (e)
of said aqueous concentrate is 55 to 65 parts per 100
by weight of concentrate, the remainder being water.

11. The composition of any of Claim 1 to 10
5 wherein the aliphatic, monobasic acid is oleic
acid, linoleic acid, caprylic acid, palmitic acid,
stearic acid, myristic acid, abietic acid or a mix-
ture thereof.

12. The composition of any of Claims 1 to 10
10 wherein the aliphatic, monobasic acid is a mixture
of tall oil fatty acids and rosin or is tallow.

13. The composition of any of Claims 1 to 12
wherein the aromatic is benzoic acid, phthalic
acid, terephthalic acid, isophthalic acid, or
15 trimellitic acid.

14. A metal object coated with the corrosion
inhibiting composition of any one of Claims 1 to 14.



European Patent
Office

EUROPEAN SEARCH REPORT

0020042
Application number
EP 80301531.2

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl. 3)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
X	GB - A - 1 415 638 (EXXON RESEARCH) * Pages 1,2; example 1; claims *	1,5-7, 11,13, 14	C 23 F 11/14
	GB - A - 1 177 873 (FUJI IRON & STEEL) * Claims *	1,5,11 12,14	
	US - A - 3 573 225 (M.KONDO) * Claims *	1,5,11 13,14	
	& DE-B-1 696 147		TECHNICAL FIELDS SEARCHED (Int.Cl. 3)
			C 23 F
		CATEGORY OF CITED DOCUMENTS	
		X: particularly relevant A: technological background O: non-written disclosure P: intermediate document T: theory or principle underlying the invention E: conflicting application D: document cited in the application L: citation for other reasons	
		&: member of the same patent family, corresponding document	
The present search report has been drawn up for all claims			
Place of search	Date of completion of the search	Examiner	
VIENNA	10-07-1980	SLAMA	

EPO Form 1503.1 08.78



Europäisches Patentamt
European Patent Office
Office européen des brevets

Publication number:

0020 042
A3

12

EUROPEAN PATENT APPLICATION

21 Application number: 80301531.2

51 Int. Cl. 2: **C 23 F 11/14**

22 Date of filing: 09.05.80

30 Priority: 09.05.79 US 37418
10.04.80 US 138758

71 Applicant: Conner Sr., Alvin J., 19 Charlotte Drive, New Orleans, Louisiana 70122 (US)

43 Date of publication of application: 10.12.80
Bulletin 80/25

72 Inventor: Conner Sr., Alvin J., 19 Charlotte Drive, New Orleans, Louisiana 70122 (US)

84 Designated Contracting States: AT BE DE FR GB IT NL
SE

88 Date of deferred publication of search
report: 07.01.81 Bulletin 81/1

74 Representative: Collier, Jeremy Austin Grey, J.A. Kemp &
Co. 14, South Square Gray's Inn, London WC1R 5EU
(GB)

54 Non-petroleum based metal corrosion inhibitor and a metal object coated therewith.

57 A non-petroleum based metal corrosion inhibitor is provided in the form of a solution of compounds mixed together in particular proportions to form a non-petroleum based coating for preventing, or inhibiting, the oxidation of metals. The solution is prepared from aliphatic mono-basic acids, aromatic acids, amines and water, with or without a lubricant. A coating of the solution inhibits oxidation of metal surfaces, provides lubricity and need not be removed from a metal surface prior to painting.

EP 0 020 042 A3

ACTURUM AG

**This Page is Inserted by IFW Indexing and Scanning
Operations and is not part of the Official Record**

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

- ☐ **BLACK BORDERS**
- ☐ **IMAGE CUT OFF AT TOP, BOTTOM OR SIDES**
- ☐ **FADED TEXT OR DRAWING**
- ☐ **BLURRED OR ILLEGIBLE TEXT OR DRAWING**
- ☐ **SKEWED/SLANTED IMAGES**
- ☐ **COLOR OR BLACK AND WHITE PHOTOGRAPHS**
- ☐ **GRAY SCALE DOCUMENTS**
- ☐ **LINES OR MARKS ON ORIGINAL DOCUMENT**
- ☐ **REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY**
- ☐ **OTHER:** _____

IMAGES ARE BEST AVAILABLE COPY.

As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.